

SAILING.

CENTRE OF LATERAL RESISTANCE.

The centre of lateral resistance is the centre of application of resistance of the water; and as this varies in position with the speed of the ship, &c., it is not determinate, but a point is generally taken at the centre of the immersed longitudinal vertical middle plane of the vessel as sufficiently accurate.

CENTRE OF EFFORT.

The point in the longitudinal vertical middle plane of a vessel which is traversed by the resultant of the pressure of the wind on the sails is termed the centre of effort; its position varies according to the quantity of sail spread, &c., but its position is determined approximately for purposes connected with designing the sails, all plain sail only being taken—that is, the sails that are more commonly used, and which can be carried with safety in a fresh breeze (see table, p. 200). They are as follows:—

In square-rigged vessels: the fore and main courses, fore, main, and mizen topsails, fore, main, and mizen topgallant sails, driver, jib, and sometimes the fore topmast staysail.

In fore and aft rigged vessels: the main sail, fore sail, and sometimes the second or third jib.

In calculating the position of the centre of effort by the following rules the sails are taken braced right fore and aft.

To find the perpendicular height of the centre of effort above the centre of lateral resistance.

RULE.—Multiply the area of each sail by the height of its centre of gravity above the centre of lateral resistance; take the sum of those products (or moments) and divide it by the total area of sail: the quotient will be the required result.

To find the lateral position of the centre of effort relatively to the centre of lateral resistance.

RULE 1.—Multiply the area of each sail whose centre lies to one side of a vertical axis passing through the centre of lateral resistance by the perpendicular distance of its centre from that axis, and add the products (or moments) together.

RULE 2.—Treat the other sails whose centres lie to the other side of the axis of moments in the same way as before, and add their products together.

The difference between the two sums added together, and divided by the total area of sail, will give the perpendicular distance of the centre of effort from the given axis.

Note.—The centre of effort will lie to that side which has the greatest moment of sail.

The following table shows the method in which the centre of effort is calculated.

TABLE SHOWING METHOD OF CALCULATING THE POSITION OF THE CENTRE OF EFFORT RELATIVELY TO THE CENTRE OF LATERAL RESISTANCE.

Name of Sail	Areas	Distances of Centre of Sail		Moments		Height of Centre of Sail Above	Vertical Moments
		Before	Aft	Before	Aft		
Jib	2040	158	—	281520	—	87.3	178092
Fore course . . .	4050	78	—	315900	—	56.0	226800
" topsail	4330	78	—	337840	—	109.5	474185
" topgallant sail . .	1500	78	—	117000	—	158.8	238200
Main course . . .	5488	—	12.5	—	67600	58.3	315286.4
" topsail	5440	—	14.0	—	76160	117.3	638112
" topgallant sail . .	1881	—	15.5	—	29155.5	172.0	324582
Driver	2831.5	—	100.5	—	284565.7	62.5	176968.7
Mizen topsail . .	2645	—	78.0	—	206310	99.5	263177.5
" topgallant sail . .	902	—	79.5	—	71709	136.0	122672
	31027.5			105226.0	735500.2		2957975.6

Hght. of Centre of Effort above Centre of Lateral Resistance	=	moment 2957975.6 area 31027.5	= 95.3.
Dist. of Centre of Effort before Centre of Lateral Resistance	=	moments 1052260 - 735500.2 area 31027.5	= 10.2.

ABDENCY.

Abdency is the tendency a ship has to fly up to the wind, thus showing that the position of her centre of effort is abaft the centre of lateral resistance.

SLACKNESS.

Slackness is the tendency a ship has to fall off from the wind, thus showing that the position of her centre of effort is before the centre of lateral resistance.

RELATIVE POSITION OF CENTRE OF EFFORT AND CENTRE OF LATERAL RESISTANCE.

D = distance of centre of effort before centre of lateral resistance.

D_1 = distance of centre of effort above centre of lateral resistance.

L = length of load water-line.

A = area of load water-line.

d = distance of centre of buoyancy of ship below load water-line.

d_1 = distance of centre of lateral resistance abaft the middle of the load water-line.

d_2 = distance of centre of buoyancy before the middle of the load water-line.

$$D = \frac{L(\frac{3}{10}d_1 + d_2)}{10(d_1 + d_2)} \text{ for square-rigged vessels.}$$

$$D = \frac{L}{10(d_1 + d_2)} \text{ for cutter and fore and aft rigged vessels.}$$

$$D_1 = \frac{4A}{5d}$$

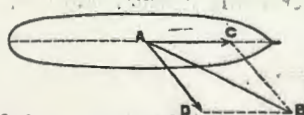
Note.—The centre of effort of the sails, to produce the best effect, must be higher or lower according as the ship is more or less full at the load water-line compared with the fulness of the body at the extremities below the water. Ships that are full at the load water-line and clean below at the extremities require the higher masts.

REAL AND APPARENT MOTION OF THE WIND.

By the real motion of the wind is meant its motion relatively to the earth, and by its apparent motion its motion relatively to the ship when she is sailing.

The apparent motion being the resultant of the real motion of the wind and of a motion equal and directly opposite to that of the ship.

FIG. 147.



DA will represent in magnitude and direction the apparent motion of the wind.

In fig. 147 let AB represent in magnitude and direction the real motion of the wind, and AC the direction and velocity of the motion of the ship; through B draw BD parallel and equal to AC ; join DA : then

In algebraical symbols let—

a = angle ADB made by the point from which the apparent wind blows with the course of the ship.

$K = 180 - a$ = supplement of ADB , the corresponding angle for the real wind.

$r = \frac{AD}{DB}$ = ratio of velocity of apparent wind to that of the ship.

$r_1 = \frac{AB}{DB}$ = ratio of velocity of real wind to that of the ship.

$$r = \{\sqrt{(r_1^2 - 1 + \cos^2 a)} + \cos a\}.$$

$$\text{When } a \text{ is obtuse, } r = \{\sqrt{(r_1^2 - 1 + \cos^2 a)} - \cos a\}.$$

$$r = \sqrt{(1 + r_1^2 + 2r_1 \cos K)}.$$

$$\text{When } K \text{ is obtuse, } r = \sqrt{(1 + r_1^2 - 2r_1 \cos K)}.$$

$$r_1 = \sqrt{(1 + r^2 - 2r \cos a)}.$$

$$\text{When } a \text{ is obtuse, } r = \sqrt{(1 + r^2 + 2r \cos a)}.$$

$$\sin K = \frac{r}{r_1} \sin a.$$

$$\sin a = \frac{r_1}{r} \sin K.$$

EFFECTIVE IMPULSE OF WIND.

D = direct impulse of wind on sails in lbs.

E = effective impulse of wind on sails in lbs.

C = component of effective impulse which produces leeway and tends to heel the ship over.

C_1 = component of effective impulse which moves the ship ahead.

θ = angle made by direction of apparent motion of wind with the plane of the sails (see fig. 148).

a = angle made by the plane of the sails with the ship's course (see fig. 148).

$$E = D \sin^2 \theta. \quad C = E \cos a. \quad C_1 = E \sin a.$$

In fig. 148 let PC represent in magnitude and direction the pressure of the apparent wind on the sail AB ; through P draw PR parallel to AB ; through C draw CR perpendicular to PR and cutting PR in R :

then RC is the effective pressure of the wind on the sail AB , and RN perpendicular to KM is the component of RC which produces heel and leeway, while NC is the component of RC which propels the ship along.

FIG. 148.



TABLE OF DIRECT IMPULSE OF WINDS IN LBS. PER SQUARE FOOT, AND SAILS COMMONLY SET BY THE WIND.

Velocity in Knots per Hour	Impulse in lbs.	Name of Wind	Sails commonly set by the Wind
1	.0067	Light air	Courses, topsails, topgallant sails, royals, spanker, jib, flying jib, and all light sails.
2	.027		
3	.060		
4	.107	Light breeze	
5	.167		
6	.240		
7	.327	Moderate breeze	
8	.427		
9	.540		
10	.667	Fresh breeze	Royals and flying jib taken in in a sea way to two reefs in the topsails.
11	.807		
12	.960		
13	1.13	Strong breeze	Single-reefed topsails and topgallant sails in much sea, two reefs in the topsails to taking in topgallant sails.
14	1.31		
15	1.50		
16	1.71		
17	1.93		
18	2.16		
19	2.41		
20	2.67	Moderate gale	Double-reefed topsails to treble-reefed topsails, reefed spanker and jib.
22	3.23		
24	3.84		
26	4.51	Fresh gale	Close-reefed topsails, reefed courses to taking in spanker, jib, fore and mizen topsails.
28	5.23		
30	6.00		
32	6.83	Strong gale	Reefed courses, close-reefed main topsail, fore staysail, mizen topsail to taking in the main sail.
34	7.71		
36	8.64		
38	9.63	Heavy gale	Close-reefed main topsail to storm staysails, or close-reefed main topsail only.
40	10.7		
45	13.5	Storm	
50	16.7		
60	24.0		
70	32.7	Hurricane	
80	42.7		
90	54.0		
100	66.7		

IMPULSE OF WIND.

v = velocity of wind in knots per hour.

D = direct impulse in lbs. on one square foot.

$$D = \frac{v^2}{150} = v^2 \cdot 006667.$$

SPEED OF SIMILAR VESSELS UNDER SAIL.

v = velocity of ship.

D = displacement of ship.

x = area of midship section.

A = area of sails.

c and c₁ = constants obtained from similar vessels.

$$v = c \sqrt{\frac{A}{x}} = c_1 \sqrt{\frac{A}{D}}$$

$$c_1 = \sqrt{\frac{v^2 D}{A}}$$

$$c = \sqrt{\frac{v^2 x}{A}}$$

$$A = \frac{v^2 x}{c^2} = \frac{v^2 D}{c_1^2}$$

TABLE OF THE RATIO OF A SHIP'S SPEED UNDER SAIL TO SPEED OF REAL WIND.

Ratio of Area of Sails to Augmented Surface	Relation between Course and Wind	Probable Ratio of Speed of Ship to Sp. of Real Wind
1	Course 5 points near wind	1.47
	Wind 2 points abaft beam	1.55
	Course 6 points near wind	1.64
	Wind abeam	1.72
1½	Wind astern	1.81
2	Course 5 points near wind	1.90
	Wind 2 points abaft beam	1.99
2½	Course about 6½ points near wind	2.08
	Wind on quarter	—

TABLE OF THE RATIO OF THE PROBABLE SPEED OF VESSELS UNDER STEAM AND CANVAS TO THOSE UNDER STEAM.

Speed under canvas + speed under steam	Probable speed under steam and canvas + speed under steam	Speed under canvas + speed under steam	Probable speed under steam and canvas + speed under steam
.4	1.02	1.3	1.47
.5	1.04	1.4	1.55
.6	1.07	1.5	1.64
.7	1.10	1.6	1.72
.8	1.15	1.7	1.81
.9	1.20	1.8	1.90
1.0	1.26	1.9	1.99
1.1	1.33	2.0	2.08
1.2	1.40	—	—

HEELING MOMENT OF SAILS.

E = effective impulse of wind on sails in lbs. (see p. 199).
 D = displacement of vessel in lbs.

C = height of centre of effort above centre of lateral resistance.

G = height metacentre above centre of gravity.

L = length of arm of righting couple at a given angle of heel.

M = heeling moment of sails.

α = angle made by plane of sails with course of ship (see fig. 148).

θ = angle of heel of vessel.

$$M = C \cdot E \cdot \cos \alpha \cdot \cos \theta.$$

The steady angle of heel of a vessel due to M will be that at which

$$M = D \cdot G \cdot \sin \theta \text{ (for small angles of heel),}$$

$$M = L \cdot D \text{ (for any angle of heel).}$$

In the two last formulae the reduction in the effective heeling power of the wind due to the sails being inclined from the upright position has been neglected, but if necessary the diminution of the effective pressure of the wind may be taken to vary as the sine squared of the angle of incidence of the wind with the plane of the ship's sails, or as the cosine squared of the angle of heel.

Note.—In a general sense the moment of sail is usually understood to be the product of the area of all plain sail into the height of the centre of effort above the centre of lateral resistance, as the pressure of wind is generally taken as one pound in the square foot; and the product of the weight of the ship in lbs. into the height of the metacentre above the centre of gravity, divided by the moment of sail, is taken as a measure of her efficiency to resist inclination under canvas.

AREA OF SAIL.

To determine accurately the quantity of sail suitable for any vessel to carry, make the moment of sail equal to the moment of stability at a definite angle of heel; but the following rule may generally be taken as sufficiently approximate:—

A = quantity of sail suitable to a given vessel.

D = displacement of vessel in lbs.

M = height of metacentre above centre of gravity.

H = height of centre of effort above centre of lateral resistance.

θ = angle of heel in circular measure suitable to given vessel taken from the following table.

$$D \times M \times \theta$$

$$- A = \frac{D \times M \times \theta}{H}$$

TABLE OF ANGLE OF STEADY HEEL FOR DIFFERENT CLASSES OF VESSELS.

Class of Vessel	Angle of Heel	Circular Measure
Frigates and large merchant ships	4°	·070
Corvettes	5°	·087
Schooners and cutters	6°	·105
Yachts	6° to 9°	·105 to ·107

TABLE OF THE AREA AND MOMENT OF SAILS OF SOME OF HER MAJESTY'S SCREW VESSELS.

	A	B	C	D	E	F	G	H
						ft. in.		
Achilles	30133	22·6	3·11	95·99	23·33	26 10	1·517	3·088
Bellerophon	23792	19·34	3·15	85·64	26·1	24 8½	2·03	3·28
Favourite	16206	20·62	5·01	105·4	21·2	21 4	1·00	3·40
Hercules	28882	21·62	3·26	118·42	18·9	24 0½	1·38	2·69
Inconstant	26034	27·57	4·61	147·9	15·1	23 10½	1·42	2·80
Iron Duke	25054	23·92	4·25	128·96	17·3	22 0	·66	3·012
Monarch	27700	22·52	3·35	129·12	17·3	24 1½	·76	2·37
Minotaur	32377	24·23	3·10	74·50	30·0	26 8½	1·999	3·879
Penelope	17168	22·32	3·93	84·35	26·6	16 6½	1·35	3·52
Prince Consort	22459	18·85	3·36	43·28	51·7	25 5	2·15	6·01
Sultan	28258	20·42	3·07	112·84	19·8	26 0	2·35	2·64
Swiftsure	25095	21·95	3·82	116·0	19·3	24 10½	1·8	3·05
Valiant	21426	17·49	3·18	59·10	37·9	25 8	1·89	4·61
Vixen	7860	22·98	6·39	74·67	29·9	11 2½	·95	4·21
Warrior	28809	23·07	3·16	63·22	35·4	26 5½	2·285	4·678

In the above table—

A = area of plain sail in square feet.

B = proportion of sail to one foot of midship section at load draught.

C = proportion of sail to one ton of displacement at load draught.

D = moment of sail about centre of lateral resistance divided by displacement in tons into the distance between the metacentre and the centre of gravity in feet.

E = weight of the ship in lbs. multiplied by the distance between the metacentre and the centre of gravity, and the product divided by the moment of sail about the centre of lateral resistance.

Note.—This is a measure of the power of a ship to resist inclination under her canvas.

F = mean load-draught of water in feet and inches.

G = distance of centre of gravity below load water-line in feet.

H = height of metacentre above centre of gravity in feet.

EFFECT OF GUST OF WIND ON A SHIP'S SAILS.

The effect of a sudden gust of wind upon a ship's sails is, as a rule, to heel her over to an extreme angle of heel of about twice the steady angle at which the same constant pressure of wind would keep her.

In fig. 149 let ABC be the ship's curve of statical stability, and DE her curve of varying moments of sail—that is, the ordinates which express the moment of sail at the different angles vary as the cosine² of the angle of heel.

FIG. 149.



If the wind is steadily applied the ship will remain inclined at a steady angle of heel of 20° , determined by dropping an ordinate at the point of intersection E of the two curves; but in the case of the same pressure of wind being suddenly applied she will heel over beyond the steady angle of heel, and she will oscillate for a time about that angle, the reason being that an amount of mechanical work has been done in heeling her over to 20° , which is represented by the area $ADEH$, whereas the work absorbed is only equal in area to $ADEH$; hence mechanical work has been accumulated equal to the area AED . The ship will therefore continue to heel over till this work has been absorbed; this will occur at 40° , when the area EKL is equal to the area AED , or, in other words, when the area ALM —the dynamical stability at 40° —is equal to the area $ADEM$ —the work which will commence a return oscillation under the influence of the righting moment, represented by KL .

TIME AND KNOT TABLE.
The number in this table corresponding to the time in which a vessel passes over the measured knot is her rate in knots per hour.

Secs.	2 min.	3 min.	4 min.	5 min.	6 min.	7 min.	8 min.	9 min.	10 min.	11 min.	12 min.	13 min.	14 min.
0	30-000	20-000	15-000	12-000	10-000	8-571	7-500	6-567	6-000	5-455	5-000	4-615	4-286
1	29-752	19-890	14-938	11-960	9-972	8-551	7-484	6-554	5-990	5-446	4-993	4-609	4-281
2	29-508	19-780	14-876	11-921	9-945	8-531	7-469	6-542	5-980	5-438	4-986	4-604	4-275
3	29-268	19-672	14-815	11-881	9-917	8-511	7-453	6-530	5-970	5-430	4-979	4-598	4-270
4	29-032	19-565	14-754	11-842	9-890	8-491	7-438	6-518	5-960	5-422	4-972	4-592	4-265
5	28-800	19-459	14-694	11-803	9-863	8-471	7-423	6-506	5-950	5-414	4-965	4-586	4-260
6	28-571	19-355	14-634	11-765	9-836	8-451	7-407	6-593	5-941	5-405	4-959	4-580	4-255
7	28-346	19-251	14-575	11-726	9-809	8-431	7-392	6-581	5-931	5-397	4-952	4-574	4-250
8	28-125	19-149	14-516	11-688	9-783	8-411	7-377	6-569	5-921	5-389	4-945	4-568	4-245
9	27-907	19-048	14-458	11-650	9-756	8-392	7-362	6-557	5-911	5-381	4-938	4-563	4-240
10	27-692	18-947	14-400	11-613	9-730	8-372	7-347	6-545	5-902	5-373	4-931	4-557	4-235
11	27-481	18-848	14-343	11-576	9-704	8-353	7-332	6-534	5-892	5-365	4-925	4-551	4-230
12	27-273	18-750	14-286	11-538	9-677	8-333	7-317	6-522	5-882	5-357	4-918	4-545	4-225
13	27-068	18-653	14-229	11-502	9-651	8-314	7-302	6-510	5-873	5-349	4-911	4-540	4-220
14	26-866	18-557	14-173	11-465	9-626	8-295	7-287	6-498	5-863	5-341	4-905	4-534	4-215
15	26-667	18-461	14-118	11-429	9-600	8-276	7-273	6-486	5-854	5-333	4-898	4-528	4-210
16	26-471	18-367	14-062	11-393	9-574	8-257	7-258	6-475	5-844	5-325	4-891	4-523	4-206
17	26-277	18-274	14-008	11-356	9-549	8-238	7-243	6-463	5-835	5-318	4-885	4-517	4-201
18	26-087	18-182	13-953	11-321	9-524	8-219	7-229	6-452	5-825	5-310	4-878	4-511	4-196
19	25-899	18-090	13-900	11-285	9-499	8-200	7-214	6-440	5-816	5-302	4-871	4-506	4-191
Secs.	2 min.	3 min.	4 min.	5 min.	6 min.	7 min.	8 min.	9 min.	10 min.	11 min.	12 min.	13 min.	14 min.

TABLE OF FACTORS USED TO DETERMINE THE LENGTHS OF MASTS AND SPARS FOR FULL-RIGGED SHIPS
(continued).

SPECIES OF MASTS AND SPARS		Clipper Ships		Screw Vessels				
				Ironclad Frigates		Wood-sheathed Corvette	Troop-ship	Merchant Steamer
		Ex. 1	Ex. 2	Ex. 1	Ex. 2			
Mizen royal mast pole	= hounded length	×	454	—	190	300	085	208
" skysail mast hounded	= main skysail mast hounded	×	—	846	—	—	—	—
" pole	= hounded length	×	—	090	—	—	—	—
Main yard.	Whole length	×	353	858	278	284	291	268
Yard arms, each	= length on water-line	×	087	036	041	044	042	050
Fore yard.	Whole length	×	1000	1000	1000	1000	1000	1000
Yard arms, each	= main yard	×	037	036	041	044	042	050
Mizen yard.	Whole length	×	789	857	676	744	701	755
Yard arms, each	= main yard	×	038	038	042	094	042	067
Main lower topsail yard	= main yard	×	843	877	—	—	—	—
Yard arms, each	= yard	×	024	052	—	—	—	—
Fore lower topsail yard	= main lower topsail yard	×	1000	1000	—	—	—	—
Yard arms, each	= yard	×	024	052	—	—	—	—
Mizen lower topsail yard	= main lower topsail yard	×	770	829	—	—	—	—
Yard arms, each	= yard	×	026	053	—	—	—	—
Main upper topsail yard	= main yard	×	919*	933*	705	744	750	800
Yard arms, each	= yard	×	052	032	081	094	085	078
Fore upper topsail yard	= main upper topsail yard	×	1000	1000	1000	1000	1000	1000
Yard arms, each	= yard	×	052	032	081	081	085	078
Mizen upper topsail yard	= main upper topsail yard	×	808	794	696	672	729	687
Yard arms, each	= yard	×	038	040	082	061	083	079
Main topgallant yard	= main upper topsail yard	×	816	816	622	672	678	641
Yard arms, each	= yard	×	049	039	043	061	042	061

* Main lower topsail yard.

TABLE OF FACTORS USED TO DETERMINE THE LENGTHS OF MASTS AND SPARS FOR FULL-RIGGED SHIPS
(concluded).

SPECIES OF MASTS AND SPARS		Clipper Ships		Screw Vessels				
				Ironclad Frigates		Wood-sheathed Corvette	Troop-ship	Merchant Steamer
		Ex. 1	Ex. 2	Ex. 1	Ex. 2			
Fore topgallant yard	= main topgallant yard	×	900	1000	1000	1000	1000	1000
Yard arms, each	= yard	×	049	039	043	061	042	061
Mizen topgallant yard	= main topgallant yard	×	774	762	728	711	737	732
Yard arms, each	= yard	×	035	040	042	089	044	042
Main royal yard	= main topgallant yard	×	818	742	706	667	737	732
Yard arms, each	= yard	×	047	040	042	042	044	042
Fore royal yard	= main royal yard	×	1000	1000	1000	1000	1000	1000
Yard arms, each	= yard	×	047	040	042	042	044	042
Mizen royal yard	= main royal yard	×	737	76	754	717	779	733
Yard arms, each	= yard	×	045	034	042	046	040	045
Main skysail yard	= main royal yard	×	—	773	—	—	—	—
Yard arms, each	= yard	×	—	031	—	—	—	—
Fore skysail yard	= main skysail yard	×	—	1000	—	—	—	—
Yard arms, each	= yard	×	—	031	—	—	—	—
Mizen skysail yard	= main skysail yard	×	—	690	—	—	—	—
Yard arms, each	= yard	×	—	037	—	—	—	—
Spanker gaff.	Whole length	×	677	785	700	700	670	660
" boom.	= spanker boom	×	216	216	184	199	197	166
Bowsprit, outside stem	= length of vessel	×	103	102	129	102	075	099
Jibboom, housing excluded	" " bowsprit	×	1768	1909	1000	1415	2250	1813
Housing	" " jibboom	×	527	524	337	348	466	552
Fore mast before after sternpost	= " " water-line	×	771	779	575	774	826	777
Main	" " "	×	452	463	425	480	441	335
Mizen	" " "	×	190	174	161	164	161	117

TABLE OF FACTORS USED TO DETERMINE THE LENGTHS OF MASTS AND SPARS FOR BARQUES AND BRIGS.

SPECIES OF MASTS AND SPARS				Screw Steam Vessels						Sailing Merchant Vessel. Barque-rigged			
				Ironclad Frigates. Barque-rigged		Merchant Vessels. Barque-rigged		Troop-ship. Barque-rigged	Merchant Vessel. Brig-rigged				
				Ex. 1	Ex. 2	Ex. 1	Ex. 2						
Main mast hounded	..	..	= breadth of vessel	..	..	x	1-125	1-126	1-410	1-606	1-102	1-395	1-577
" " headed	..	..	= hounded length	..	..	x	254	317	264	245	278	204	276
Fore " hounded	..	..	= main mast hounded	..	..	x	913	905	927	898	908	943	928
" " headed	..	..	= hounded length	..	..	x	278	351	282	272	286	280	298
Mizen " hounded	..	..	= main mast hounded	..	..	x	873	873	837	979	1-056	—	928
" " headed	..	..	= hounded length	..	..	x	230	228	231	167	175	—	211
Main topmast hounded	..	..	= breadth of vessel	..	..	x	687	857	1-000	1-000	820	1-052	1-267
" " headed	..	..	= hounded length	..	..	x	—	—	179	167	134	175	167
Fore " hounded	..	..	= main topmast hounded	..	..	x	1-000	1-000	1-000	1-000	1-000	1-000	1-000
" " headed	..	..	= hounded length	..	..	x	—	—	179	167	134	175	167
Mizen " hounded	..	..	= main topmast hounded	..	..	x	1-247	1-000	821	1-567	1-093	—	1-289
" " pole	..	..	= hounded length	..	..	x	188	188	344	086	159	—	207
Main topgallant mast hounded	..	..	= breadth of vessel	..	..	x	393	250	615	623	459	631	690
" " " pole	..	..	= hounded length	..	..	x	114	071	500	—	—	667	—
Fore " " hounded	..	..	= main topgallant mast hounded	..	..	x	1-000	1-000	1-000	1-000	1-000	1-000	1-000
" " " pole	..	..	= hounded length	..	..	x	114	071	500	—	—	667	—
Main royal mast hounded	..	..	= breadth of vessel	..	..	x	—	—	—	475	286	—	408
" " " pole	..	..	= hounded length	..	..	x	—	—	—	310	143	—	138
Fore " " hounded	..	..	= main royal mast pole	..	..	x	—	—	—	1-000	1-000	—	1-000
" " " pole	..	..	= hounded length	..	..	x	—	—	—	310	143	—	138
Main yard.	Whole length	..	= length of water-line	..	..	x	205	325	224	311	217	260	382
Fore yard.	Yard arms, each	..	= yard	..	..	x	067	050	066	043	044	004	047
	Whole length	..	= main yard	..	..	x	1-000	1-000	1-000	1-000	1-000	1-000	1-000
	Yard arms, each	..	= yard	..	..	x	067	050	066	043	044	004	047

TABLE OF FACTORS USED TO DETERMINE THE LENGTHS OF MASTS AND SPARS FOR BARQUES AND BRIGS (concluded).

SPECIES OF MASTS AND SPARS				Screw steam Vessels								Sailing Merchant Vessel. Barque-rigged
				Ironclad Frigates. Barque-rigged		Merchant Vessels. Barque-rigged		Troop-ship. Barque-rigged	Merchant Vessel. Brig-rigged			
				Ex. 1	Ex. 2	Ex. 1	Ex. 2					
Main topsail yard . . .	= main yard . . .	x	719	736	760	785	812	743	762			
Yard arms, each . . .	= yard . . .	x	055	074	105	073	077	086	078			
Fore topsail yard . . .	= main topsail yard . . .	x	1000	1000	1000	1000	1000	1000	1000			
Yard arms, each . . .	= yard . . .	x	055	074	105	073	077	086	078			
Mizen gaff topsail yard . . .	= spanker gaff . . .	x	540	543	*	—	591	*	—			
Yard arms, each . . .	= yard . . .	x	100	100	—	—	095	—	—			
Main topgallant yard . . .	= main topsail yard . . .	x	628	657	631	690	700	689	656			
Yard arms, each . . .	= yard . . .	x	068	068	083	066	045	050	048			
Fore topgallant yard . . .	= main topgallant yard . . .	x	1000	1000	1000	1000	1000	1000	1000			
Yard arms, each . . .	= yard . . .	x	068	068	083	066	045	050	048			
Main royal yard . . .	= main topgallant yard . . .	x	—	—	—	684	791	—	714			
Yard arms, each . . .	= yard . . .	x	—	—	—	058	041	—	042			
Fore royal yard . . .	= main royal yard . . .	x	—	—	—	1000	1000	—	1000			
Yard arms, each . . .	= yard . . .	x	—	—	—	058	041	—	042			
Spanker gaff. Whole length boom . . .	= spanker boom . . .	x	661	661	625	700	670	133†	145†			

† Jib-headed topsail.

† Spanker gaff = length of vessel x.

TABLE OF FACTORS USED TO DETERMINE THE LENGTHS OF MASTS AND SPARS OF SCHOONERS AND BRIGS.

SPECIES OF MASTS AND SPARS				Screw Steam Vessels								Merchant Sailing Vessel, Brig-rigged
				Ironclads		Ship of War, Schooner-rigged	Merchant Vessels					
				3-masted Schooner	Schooner-rigged		3-masted Schooner	Schooner-rigged	Schooner-rigged	Fore and Aft Schooner		
Fore mast hounded	= breadth of vessel	x	1-125	1-127	1-634	1-467	1-950	2-133	1-753	1-740		
" " headed	= hounded length	x	222	237	235	230	205	202	—	218		
Main " hounded	= fore mast hounded	x	1-089	1-125	1-035	1-068	1-051	1-027	1-057	1-172		
" " headed	= hounded length	x	204	211	230	213	195	200	—	186		
Mizen " hounded	= fore mast hounded	x	911	—	—	848	—	—	—	—		
" " headed	= hounded length	x	171	—	—	173	—	—	—	—		
Fore topmast hounded	= breadth of vessel	x	675	76	807	850	800	1500	1333	1368		
" " headed	= hounded length	x	—	—	—	—	—	—	—	140		
" " pole	= " " "	x	—	—	—	—	—	115	150	—		
Main " hounded	= fore topmast hounded	x	1-426	1-370	1-738	1-608	1-75	1-04	1-000	1368		
" " headed	= hounded length	x	—	—	—	—	—	—	—	140		
" " pole	= " " "	x	170	185	100	146	143	112	200	—		
Mizen " hounded	= fore topmast hounded	x	1-148	—	—	100	—	—	—	—		
" " pole	= hounded length	x	161	—	—	200	—	—	—	—		
Fore topg. mast hounded	= breadth of vessel	x	340	394	481	533	500	—	—	600		
" " pole	= hounded length	x	185	111	236	312	400	—	—	—		
Main " " hounded	= fore topg. mast hounded	x	—	—	—	—	—	—	—	1-067		
Fore royal	= breadth of vessel	x	—	—	—	—	—	—	—	367		
" " pole	= hounded length	x	—	—	—	—	—	—	—	235		
Main " " hounded	= fore royal mast hounded	x	—	—	—	—	—	—	—	1-117		
" " pole	= hounded length	x	—	—	—	—	—	—	—	211		
Fore yard. Whole length	= length of vessel	x	900	265	400	310	354	380	—	450		
Yard arms, each	= yard	x	650	665	660	660	643	661	—	648		

SPECIES OF MASTS AND SPARS				Screw Steam Vessels							Merchant Sailing Vessel, Brig-rigged
				Ironclads		Ship of War, Schooner-rigged	Merchant Vessels			Fore and Aft Schooner	
				3-masted Schooner	Schooner-rigged		3-masted Schooner	Schooner-rigged	Schooner-rigged		
Main yard.	Whole length	= fore yard	x	—	—	—	—	—	—	—	1-072
	Yard arms, each	= yard	x	—	—	—	—	—	—	—	045
Fore topsail yard.	Whole length	= fore yard	x	683	647	741	754	739	585	*	705
	Yard arms, each	= yard	x	073	076	090	092	074	083	—	055
Main topsail yard.	Whole length	= fore tops. yard	x	—	—	—	—	—	—	—	1-055
	Yard arms, each	= yard	x	—	—	—	—	—	—	—	055
Main gaff topsail yard.	Whole length	= main gaff	x	690	617	412	542	667	709	702	—
Mizen	"	= mizen gaff	x	583	—	—	574	—	—	—	—
Fore topgallant yard.	Whole length	= fore tops. yard	x	683	683	655	661	653	—	—	705
	Yard arms, each	= yard	x	063	074	073	072	071	—	—	035
Main topgallant yard.	Whole length	= fore topg. yard	x	—	—	—	—	—	—	—	1-040
	Yard arms, each	= yard	x	—	—	—	—	—	—	—	035
Fore royal yard.	Whole length	= fore topg. yard	x	—	—	—	—	—	—	—	756
	Yard arms, each	= yard	x	—	—	—	—	—	—	—	050
Main royal yard.	Whole length	= fore royal yard	x	—	—	—	—	—	—	—	1-128
	Yard arms, each	= yard	x	—	—	—	—	—	—	—	050
Fore gaff.	Whole length	= lgth. of vessel	x	145	121	206	152	146	231	223	317
Main "	"	= fore gaff	x	1-000	1-214	1-100	1-127	1-142	1-060	1-088	1-000
Mizen	"	= " "	x	837	—	—	871	—	—	—	—
Spanker boom.	Whole length	= mizen gaff	x	1-416	1-53	1-560	1-425	1-700	1-056	1-513	†
Bowsprit, exclusive of housing.	"	= lgth. of vessel	x	080	105	187	105	100	200	191	213
Jibboom	"	= " jibb.	x	2-562	—	—	1-000	1-230	—	—	1-728
Distance of fore mast bef. rudder post	"	= " vessel	x	705	721	760	767	711	754	750	756
" main	"	= " "	x	330	298	303	433	315	317	316	345
" mizen	"	= " "	x	115	—	—	141	—	—	—	—

* Fore gaff topsail yard = fore gaff x .647

† Main boom = main gaff x 1.523.

TABLE OF FACTORS USED TO DETERMINE THE DIAMETERS OF SHIPS' MASTS AND SPARS.

SPECIES OF MASTS AND SPARS		Given Diamr. = Whole Length x	End Diameters = Given Diameter x
Lower masts	Ships', brigs', and barques'.	.025 to .028	heel .833 hounds .800 head .753
	Cutters'	.020 " .021	heel .833 hounds .750 head .500
	Schooners'	.020 " .022	heel .833 hounds .800 head .679
	Luggers'	.020 " .021	heel .833 hounds .750 head .583
Topmasts	Ships', brigs', and barques'.	.028 " .025	hounds .800 head .679 hounds .771
	Cutters' and schooners'.	.020 " .022	hounds .771 head .500
	Luggers'	.020 " .021	hounds .771 pole .500
	Topgallant masts	.020 " .021	hounds .771 sky-sail pole .500
Bowsprit	Ships', brigs', and barques'.	.040 " .050	heel .833 head .666
	Cutters' and schooners'.	.040 " .050	heel .833 head .666
	Lower yard	.020 " .025	yard arms .500
	Top-sail yard	.017 " .020	" .500
Yards	Topgallant and royal yard.	.017 " .018	" .500
	Cross jack yard	.020 " .025	" .500
	Cutters' and schooners' square sail	.014 " .017	" .500
	Cutters' and schooners' topsail	.017 " .020	" .500
Booms	Luggers' yards	.018 " .023	" .500
	Driver boom	.017 " .020	outer end .75 inner " .73
	Main and cutters' booms	.017 " .020	outer " .71 inner " .73
	Jibboom	.020 " .025	outer " .66 inner " .66
Gaffs	Flying jibboom	.017 " .020	outer " .73 inner " .66
	Jib and flying jibboom in one	.022 " .026	outer " .50 inner " .50
	Ships' and brigs'	.018 " .022	outer end .60
	Cutters' and schooners'	.018 " .022	" .60
	Trysail gaffs	.030 " .040	" .60

TABLE OF POSITION AND RAKE OF MASTS FOR SAILING VESSELS.

BIG AND NAMES OF MASTS		Distance from Middle of Water Line in Fractions of the Length of that Line		Rake in Twelve Feet
		Before	Aft	Inches
Frigate	{ main mast	—	.062 to .069	6 to 5
	{ fore "	.37 to .39	—	2 to 1
	{ mizen "	—	.341 to .404	10 to 9
Corvette	{ main "	—	.096 to .06	6 to 10½
	{ fore "	.372 to .399	—	2 to 1½
	{ mizen "	—	.375 to .356	10 to 10½
Clipper ship	{ main "	—	.047	1
	{ fore "	.274	—	9
	{ mizen "	—	.309	15
Lugger	{ main "	—	.04	.12
	{ fore "	.396	—	.6
	{ mizen "	—	.396	.24
Barque	{ main "	—	.067	13
	{ fore "	.300	—	11
	{ mizen "	—	.349	17
3-masted schooner	{ main "	—	.033	27
	{ fore "	.295	—	24
	{ mizen "	—	.366	30
Common schooner	{ main "	—	.046	24
	{ fore "	.338	—	15
Bermuda schooner	{ main "	—	.108 to .084	24 to 33
	{ fore "	.279 to .31	—	16 to 36
Brig of war	{ main "	—	.147 to .138	10 to 9
	{ fore "	.331 to .323	—	3 to 2
Yacht as brig	{ main "	—	.144	10
	{ fore "	.323	—	2½
Ketch	{ main "	.11	—	12
	{ mizen "	—	.395	18
Revenue cutter	{ main "	.13 to .104	—	14 to 13
	{ fore "	—	—	—
	{ mizen "	—	—	—
Cutter yacht	main "	.112 to .14	—	12 to 15

Note.—The factors in the above table will apply equally well whether the masts and spars are of wood or of iron.

TABLE OF THE WEIGHT OF VESSELS, MASTS, SPARS, RIGGING, AND SAILS IN TONS.

Kind of Vessel	Sailing Ships				
Tonnage (B.M.)	2,600	2,300	1,700	1,400	1,000
Lower masts and bowsprit*	52.6	51.9	38.7	34.1	21.6
Topmasts and yards	37.1	36.0	27.5	26.5	18.0
Spare gear and booms	16.5	16.0	12.6	12.0	7.6
Standing rigging†	22.0	21.2	20.2	19.1	11.0
Running	18.1	17.2	16.9	16.3	11.4
Blocks to	12.2	11.1	10.6	10.0	5.4
Ship's sails	6.9	7.3	6.0	5.1	3.8
Spare	4.2	4.4	3.7	3.4	2.3

Kind of Vessel	Sailing Ship	Brigs		Schooner	Cutter
Tonnage (B.M.)	500	380	230	180	160
Lower masts and bowsprit	9.1	7.5	4.3	6.4	5.5
Topmasts and yards	8.8	7.2	5.8	1.9	2.6
Spare gear and booms	4.1	3.0	2.2	1.2	—
Standing rigging†	9.4	3.8	2.4	1.9	1.7
Running	6.5	4.5	2.8	1.4	1.3
Blocks to	4.2	2.0	1.0	.3	.2
Ship's sails	2.1	1.5	1.2	1.3	1.6
Spare	1.5	1.2	.85	.8	.23

* The masts and spars are all of wood.

† Standing rigging of wire.

TABLE OF THE RELATIVE PROPORTIONS OF IRON AND HEMPEN CABLES, TOGETHER WITH THEIR WEIGHT.

Diam. of Chain		Girth of Hemp		Weight of 100 Fathoms		Diam. of Chain		Girth of Hemp		Weight of 100 Fathoms	
Ins.	Ins.	Ins.	Ins.	Cwt. Qr. Lb.	Cwt. Qr. Lb.	Ins.	Ins.	Ins.	Ins.	Cwt. Qr. Lb.	Cwt. Qr. Lb.
2	7½	8	8	29 0 17	12 0 26	1½	15	15½	15	110 0 14	43 0 1
	8	9	9	13 3 16	15 2 25		16	16½	16	48 3 24	51 8 3
2	9	10	10	39 1 21	17 0 22	1½	17	17½	17	136 2 10	55 1 0
	10	11	11	50 0 14	19 0 21	1½	18	18½	18	153 0 9	58 2 6
	10½	12	12		21 0 20		19	19½	19		61 3 13
	11	13	13		23 1 0		20	20½	20		65 2 1
1	11½	14	14	65 3 5	25 0 15	1½	21	21½	21	180 3 14	69 0 17
	12	15	15		27 1 23		22	22½	22	190 0 14	76 8 1
	12½	16	16		29 8 3	2	23	23½	23		84 1 14
	13	17	17	81 8 12	32 1 19	2	24	24½	24		92 9 16
	13½	18	18		35 0 7		25	25½	25		101 2 8
	14	19	19		37 2 4	2½	26	26½	26	216 0 0	110 2 1
	14½	20	20	94 0 7	40 1 12	2½	27	27½	27		119 3 2

TABLE GIVING THE GIRTHS OF HEMP AND WIRE ROPE OF EQUIVALENT STRENGTHS.

Hemp (ins.)	Wire (ins.)	Hemp (ins.)	Wire (ins.)	Hemp (ins.)	Wire (ins.)	Hemp (ins.)	Wire (ins.)	Hemp (ins.)	Wire (ins.)
12	4½	10½	4½	8½	3½	6½	2½	5	2
12½	—	10	4	8½	3½	6½	2½	4½	—
13	4½	9½	3½	8	3½	6½	2½	4½	1½
13½	—	9½	3½	7½	3½	6	2½	4½	2½
14	4½	9½	3½	7½	3½	5½	2½	4	1½
14½	—	9	3½	7½	3½	5½	2½	3½	1½
15	4½	8½	—	7	2½	5½	—	3½	1½

TABLE SHOWING FROM WHAT NUMBERS OF CANVAS THE DIFFERENT SAILS ARE MADE.

No. of Canvases	Species of Sails made of the given Number of Canvas
0	Courses, lower staysails, trysails.
1	Courses, lower staysails, trysails, awnings.
2	Courses, topsails, lower staysails, trysails, spankers, awnings.
3	Courses, topsails, spankers, jibs, lower and topmast staysails.
4	Topsails, topgallant sails, spankers, jibs, topmast staysails.
5	Topsails, lower and topmast studding sails, spankers, jibs, upper staysails, gaff topsails.
6	Topgallant sails, studding sails, jibs, flying jibs, upper staysails, gaff topsails, cutters' and schooners' crossjack sails and square topsails, sails of boats.
7	Topgallant sails, studding sails, flying jibs, royal staysails, cutters' and schooners' topsails, sails of boats.
8	Royals, skysails, topgallant and royal studding sails, cutters' and schooners' topgallant sails, sails of boats.

Note.—For the weight of the several numbers of canvas see p. 303.

WEIGHT OF SHIPS' RIGGING AND BLOCKS.

Weight of a ship's running rigging = weight of	sailing ships . 1.534
Wire standing rigging x	barques . 1.632
	brigs . 1.719
Weight of a ship's blocks = weight of running	sailing ships . .369
rigging x	barques . .302
	brigs . .254

Note.—The above constants must only be taken as rough approximations.

PROPORTIONS OF TRESTLE AND CROSS TREES IN SHIPS' TOPS.

Length of trestle-trees	=	hounded length of topmast x	.22
Breadth of ditto	=	length	x .11
Depth of ditto	=	breadth	x .67
Length of cross-trees	=	hounded length of topmast x	.31
Breadth of ditto	=	breadth of trestle-trees	x 1.0
Depth of ditto	=	breadth	x .67
Length of lubber's hole	=	length of trestle-trees	x .41
Length of fid	=	diameter of lower mast	x 1.50

TABLE SHOWING THE SIZES AND TOTAL WEIGHTS OF THE STANDING RIGGING OF SAILING VESSELS WHEN MADE OF MESSRS. R. S. NEWALL AND CO.'S PATENT IMPROVED WIRE ROPE, COMPARED WITH RIGGING MADE OF THE BEST HEMP ROPE.

SPECIES OF STANDING RIGGING	Ship, 1,300 T.		Ship, 1,150 T.		Ship, 900 T.		Ship, 750 T.		Ship, 600 T.		Ship, 500 T.		Ship, 400 T.		Bark, 300 T.		Bark, 200 T.		Brig, 270 T.	
	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire	Girth (ins.)	Hemp Wire
Fore & main shrouds	10	4	9	3	8	3	8	3	8	3	7	3	7	2	6	2	6	2	6	2
Mizen shrouds	8	3	7	3	7	3	7	3	6	2	6	2	5	2	5	2	4	2	4	2
Fore stays (double)	10	4	9	3	8	3	8	3	7	3	7	3	7	3	6	2	6	2	6	2
Main stays (double)	10	4	9	3	8	3	8	3	7	3	7	3	7	3	6	2	6	2	6	2
Mizen stay (single)	8	3	7	3	7	3	7	3	6	2	6	2	5	2	5	2	4	2	4	2
Fore & main shrouds	8	3	7	3	7	3	7	3	6	2	6	2	5	2	5	2	4	2	4	2
Mizen shrouds	6	2	5	2	5	2	5	2	4	1	4	1	3	1	3	1	3	1	3	1
Fore stays (double)	9	3	8	3	8	3	8	3	7	3	7	3	7	3	6	2	6	2	6	2
Mizen stay (single)	8	3	7	3	7	3	7	3	6	2	6	2	5	2	5	2	4	2	4	2
Main stays (double)	9	3	8	3	8	3	8	3	7	3	7	3	7	3	6	2	6	2	6	2
Mizen stay	6	2	5	2	5	2	5	2	4	1	4	1	3	1	3	1	3	1	3	1
Fore & main backstays	9	3	8	3	8	3	8	3	7	3	7	3	7	3	6	2	6	2	6	2
Mizen backstays	7	3	7	3	7	3	7	3	6	2	6	2	5	2	5	2	4	2	4	2
Fore & main shrouds	5	2	4	1	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1
Mizen shrouds	4	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1
Fore & main stays	6	2	5	2	5	2	5	2	4	1	4	1	3	1	3	1	3	1	3	1
Mizen stay	4	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1
Fore & main backstays	6	2	5	2	5	2	5	2	4	1	4	1	3	1	3	1	3	1	3	1
Mizen backstays	5	2	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1	3	1
Fore & main stays	5	2	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1	3	1
Mizen stay	4	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1
Fore & main backstays	4	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1
Mizen backstays	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1
Outer jib stay	8	3	8	3	7	3	7	3	7	3	6	2	6	2	6	2	5	2	5	2
Flying	6	2	5	2	5	2	5	2	4	1	4	1	3	1	3	1	3	1	3	1
Standing guys	9	3	8	3	8	3	8	3	7	3	7	3	7	3	6	2	6	2	6	2
Flying	6	2	5	2	5	2	5	2	4	1	4	1	3	1	3	1	3	1	3	1
Total wt. of hemp rigging	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11	Cwt. Qr. Lb.	108 9 11
wire		108 9 11		108 9 11		108 9 11		108 9 11		108 9 11		108 9 11		108 9 11		108 9 11		108 9 11		108 9 11

TABLE SHOWING THE SIZES AND TOTAL WEIGHTS OF THE STANDING RIGGING OF SAILING VESSELS WHEN MADE OF MESSRS. R. S. NEWALL AND CO.'S PATENT IMPROVED WIRE ROPE, COMPARED WITH RIGGING MADE OF THE BEST HEMP ROPE.

SPECIES OF STANDING RIGGING		3,000 Tons		2,500 Tons		2,000 Tons		1,500 Tons		1,200 Tons		1,000 Tons		800 Tons		600 Tons		350 Tons		200 Tons	
		Girth (ins.)		Girth (ins.)		Girth (ins.)		Girth (ins.)		Girth (ins.)		Girth (ins.)		Girth (ins.)		Girth (ins.)		Girth (ins.)		Girth (ins.)	
		Hemp	Wire	Hemp	Wire	Hemp	Wire	Hemp	Wire	Hemp	Wire	Hemp	Wire	Hemp	Wire	Hemp	Wire	Hemp	Wire	Hemp	Wire
Lower masts	Fore & main shrouds	10	4	10	4	10	4	10	4	10	4	9	4	9	3	8	3	6	2	6	2
	Mizen shrouds	7	3	7	3	6	3	6	3	6	3	6	2	6	2	5	2	4	1	4	1
	Fore & main stays (dbl.)	12	5	12	5	12	5	12	5	12	5	11	4	11	4	10	4	9	3	9	3
	Mizen stay (single)	7	3	7	3	7	3	7	3	6	2	6	2	6	2	5	2	4	1	4	1
	Fore & main shrouds	6	2	6	2	5	2	5	2	5	2	5	2	5	2	4	1	3	1	3	1
	Mizen shrouds	4	1	4	1	4	1	4	1	4	1	4	1	4	1	3	1	3	1	3	1
	Fore & main stays (dbl.)	9	4	9	4	9	4	9	4	9	4	8	3	8	3	7	3	6	2	6	2
	Mizen stay (single)	6	3	6	3	6	3	6	3	6	3	5	2	5	2	4	2	4	2	4	2
	Fore & main backstays	9	4	9	4	9	4	9	4	9	4	8	3	8	3	7	3	6	2	6	2
	Mizen backstays	6	3	6	3	6	3	6	3	6	3	5	2	5	2	4	2	4	2	4	2
Topmasts	Fore & main shrouds	4	1	4	1	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1
	Mizen shrouds	4	1	4	1	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1
	Fore & main stays	6	2	6	2	6	2	6	2	6	2	5	2	5	2	4	2	4	2	4	2
	Mizen stay	4	1	4	1	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1
	Fore & main backstays	6	2	6	2	6	2	6	2	6	2	5	2	5	2	4	2	4	2	4	2
	Mizen backstays	4	1	4	1	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1
	Fore & main stays	4	1	4	1	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1
	Mizen stay	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1
	Fore & main backstays	4	1	4	1	4	1	4	1	4	1	3	1	3	1	3	1	3	1	3	1
	Mizen backstays	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1	3	1
Royal masts	Standing jib stay	7	3	7	3	7	3	7	3	6	3	6	3	6	2	5	2	4	2	4	2
	Flying	5	2	5	2	5	2	5	2	4	2	4	1	4	1	3	1	3	1	3	1
	Standing guys	7	3	7	3	7	3	7	3	6	3	6	3	6	2	5	2	4	2	4	2
	Flying	5	2	5	2	5	2	5	2	4	2	4	1	4	1	3	1	3	1	3	1
	Martingale stay	5	2	5	2	5	2	5	2	4	2	4	1	4	1	3	1	3	1	3	1
	Martingale back-ropes	5	2	5	2	5	2	5	2	4	2	4	1	4	1	3	1	3	1	3	1
	Bob - (3 of wire) (single)	10	4	10	4	10	4	10	4	10	4	9	3	9	3	8	3	6	2	6	2
	stays (3 of hemp) (double)	10	4	10	4	10	4	10	4	10	4	9	3	9	3	8	3	6	2	6	2
	Bowsprit shrouds	9	4	9	4	9	4	9	4	9	4	8	3	8	3	7	3	6	2	6	2
	Jib gear																				
wire																					
Total wt. of hemp rigging		Cwt. Qr. Lb.	227 2 2	Cwt. Qr. Lb.	206 1 10	Cwt. Qr. Lb.	186 0 25	Cwt. Qr. Lb.	172 8 3	Cwt. Qr. Lb.	146 0 12	Cwt. Qr. Lb.	131 1 9	Cwt. Qr. Lb.	128 0 14	Cwt. Qr. Lb.	83 1 7	Cwt. Qr. Lb.	53 3 12	Cwt. Qr. Lb.	45 0 14
wire			147 0 0		128 0 14		119 3 1		108 3 26		86 8 4		50 1 4		37 6		21 1 5		13 2 2		7 2 2

Wire rigging is now almost universally used for the standing rigging of ships, as its advantages over that of hemp are considerable, its bulk being about only one-sixth that of hemp, while the weight is reduced to nearly one-half; it does not stretch permanently under great strains, as hemp rigging does, and neither is it liable to those sudden alterations of length to which hemp is subject by change in the state of moisture of the atmosphere, and which give rise to inconvenience and great labour in setting up the rigging.

TABLE FOR SAILING SHIPS, SHOWING THE PROPORTIONS WHICH THE DIAMETER OF CHAIN RIGGING AND THE GIRTHS OF HEMP OR WIRE RIGGING SHOULD BEAR TO THE DIAMETERS OF THE MASTS, YARDS, &c. FROM WHICH THE RIGGING LEADS.*

PARTS OF RIGGING	Ratios	PARTS OF RIGGING	Ratios
Fore and main masts		Fore and main topmasts	
Pendant	375	Braces	250
Shrouds †	168	Lifts	291
Stays †	227	Parrel rope	336
Ratlines	057	Clewlines	291
Foot-ropes	281	Buntlines	250
Stirrups	187	Bowlines	250
Lifts	250	Reef tackles	250
Braces	250	Sheets †	050
Tacks	312	Studding-sail halliards	291
Sheets	312	Sheets	272
Clew garnets	218	Tacks	291
Bowlines	250	Downhaul	167
Bridles	250	Boom jiggers	167
Buntlines	187	Heel lashing	250
Leechlines	156	Boom-brace pendant	291
Slabline	125	Whip	167
Fore staysail stay †	149	Shrouds †	194
Halliards	187	Backstays †	208
Sheets	187	Stay †	194
Tack lashing	125	Royal stay †	111
Downhaul	156	Backstay †	111
Lower studding sail		Halliards and strapping	
Halliards	187	Foot-ropes	312
Inner halliards	187	Braces and strapping	272
Sheets and tack	187	Lifts	250
Shrouds †	158	Parrel ropes	250
Ratlines	065	Clewlines	250
Backstays	186	Bowlines	250
Barton pendants	290	Bridles	250
Stays †	186	Sheets	250
Futtock shrouds	153	Studding-sail halliards	250
Ratlines	065	Sheets	250
Staysail halliards	193	Tacks	250
Downhaul	161	Downhaul	187
Pendants	290	Halliards	250
Sheets	226	Foot-ropes	250
Fore and main top-royal yards		Braces and strapping	
Topsail ties †	050	Lifts	336
Halliards	250	Parrel lashing	167
Foot-ropes	291	Clewlines & bowlines	167
Stirrups	167	Sheets	37
Flemish horses	208		

* All the rigging is of hemp, except that marked otherwise.
† Wire-rope rigging. ‡ Chain rigging.

TABLE FOR SAILING SHIPS, SHOWING THE PROPORTIONS OF CHAIN AND HEMP AND WIRE-ROPE RIGGING IN RELATION TO THE MASTS AND SPARS (concluded).*

PARTS OF RIGGING	Ratios	PARTS OF RIGGING	Ratios
Shrouds †	146	Foot-ropes	200
Burton pendants	250	Braces and strapping	200
Ratlines	069	Parrel lashing	100
Stay †	174	Lifts	800
Seizings †	027	Halliards	400
Foot-ropes	231	Sheets	200
Stirrups	200	Clewlines	200
Lifts	200	Topping lifts	450
Braces & strapping	200	Falls and strapping	300
Shrouds †	167	Boom sheet	350
Stay †	167	Outhauler	350
Ratlines	056	Guy pendants	350
Backstays †	156	Falls	250
Futtock shrouds †	156	Strapping to do	250
Topsail ties †	050	Throat halliards	400
Halliards for do.	274	Peak halliards	400
Foot-ropes	211	Vang pendants	350
Stirrups	274	Falls and strapping	200
Flemish horses	211	Peak brails	200
Parrel rope	316	Throat brails	250
Lifts	316	Middle brails	200
Braces	274	Hook brails	200
Sheets †	050	Gammoning †	028
Clewlines	211	Shrouds †	028
Buntlines	211	Bobstays †	033
Span	211	Man-ropes	150
Bowlines	211	Jibstay †	132
Bridles	211	Guy, single †	148
Reef tackles	237	Foot-ropes	214
Shrouds †	179	Martingale stay †	205
Backstays †	179	Martingale backropes †	134
Stay †	179	Halliards	232
Royal stay †	144	Downhaul	214
Backstays †	144	Sheets	178
Foot-ropes	231	Pendants	321
Parrel lashing	231	Flying jib stay †	150
Lifts	308	Guy †	125
Halliards	346	Foot-ropes	250
Sheets	308	Martingale stay †	175
Clewlines	231	Halliards and strapping	250
Bowlines	231	Downhaul and strapping	200
Bridles	231	Sheets	250
Strapping, 4-blocks	308	Heel lashing	150

* All the rigging is of hemp, except that marked otherwise.
† Wire-rope rigging. ‡ Chain rigging.

Note.—Girth of any lanyard=girth of rope set up by it x 5.

TABLE OF THE DIMENSIONS OF SHIPS' BLOCKS (in Inches).

Length of Block	Breadth of Block	Thickness of Block	Length of Mortise	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole	Length of Block	Breadth of Block	Thickness of Block	Length of Mortise	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole
3	2	1	2	1	1	1	17	12	7	13	10	2	1
4	3	2	3	2	2	2	18	13	8	14	11	2	1
5	4	3	4	3	3	3	19	14	9	15	12	3	1
6	4	4	4	4	4	4	20	14	9	15	12	3	1
7	5	5	5	5	5	5	21	15	9	16	13	3	1
8	6	6	6	6	6	6	22	16	9	17	14	3	1
9	7	7	7	7	7	7	23	16	9	17	14	3	1
10	7	7	7	7	7	7	24	17	10	18	15	3	1
11	8	8	8	8	8	8	25	17	10	19	16	3	1
12	9	9	9	9	9	9	26	18	10	19	16	3	1
13	10	10	10	10	10	10	27	19	11	20	17	3	2
14	10	10	10	10	10	10	28	19	11	21	17	3	2
15	11	11	11	11	11	11	29	20	11	22	18	3	2
16	12	12	12	12	12	12	30	21	12	22	18	3	2

Common Single-thick Blocks.

8	6	3	6	5	7	19	15	6	15	13	1	1
9	7	4	7	6	8	20	15	6	16	14	1	1
10	8	5	8	7	9	21	16	6	16	14	1	1
11	9	6	9	8	10	22	17	6	17	15	1	1
12	9	6	9	8	10	23	18	6	17	15	1	1
13	10	7	10	9	11	24	18	6	18	16	1	1
14	11	8	11	10	12	25	19	7	19	17	1	1
15	12	9	12	11	13	26	20	7	20	18	1	1
16	12	9	12	11	13	27	21	7	21	19	1	1
17	13	10	13	12	14	28	21	7	22	20	1	1
18	14	11	14	13	15	—	—	—	—	—	—	—

Common Single-thin Blocks.

5	3	2	3	2	7	13	9	7	9	6	2	1
6	4	3	4	3	8	14	9	8	10	7	3	1
7	4	3	4	3	8	15	10	8	10	8	3	1
8	5	4	5	4	9	16	10	8	11	8	3	1
9	6	5	6	5	10	17	10	8	11	8	3	1
10	7	6	7	6	11	18	11	9	12	9	3	1
11	7	6	7	6	11	19	11	9	12	9	3	1
12	8	7	8	7	12	20	12	10	13	10	3	1

Clump Blocks.

5	4	3	4	3	8	7	4	1	1	1	1
6	5	4	5	4	9	8	—	4	1	1	1
7	6	5	6	5	10	9	—	5	1	1	1

Clewline Blocks.

TABLE OF THE DIMENSIONS OF SHIPS' BLOCKS (in Inches)—continued.

Length of Block	Breadth of Block	Thickness of Block	Length of Mortise	Thickness of Mortise	Length of Mortise	Thickness of Mortise	Length of Mortise	Thickness of Mortise	Length of Mortise	Thickness of Mortise	Length of Mortise	Thickness of Mortise	Length of Mortise	Thickness of Mortise
3	2	1	2	1	1	1	17	12	7	13	10	2	1	1
4	3	2	3	2	2	2	18	13	8	14	11	2	1	1
5	4	3	4	3	3	3	19	14	9	15	12	3	1	1
6	4	4	4	4	4	4	20	14	9	15	12	3	1	1
7	5	5	5	5	5	5	21	15	9	16	13	3	1	1
8	6	6	6	6	6	6	22	16	9	17	14	3	1	1
9	7	7	7	7	7	7	23	16	9	17	14	3	1	1
10	7	7	7	7	7	7	24	17	10	18	15	3	1	1
11	8	8	8	8	8	8	25	17	10	19	16	3	1	1
12	9	9	9	9	9	9	26	18	10	19	16	3	1	1
13	10	10	10	10	10	10	27	19	11	20	17	3	2	2
14	10	10	10	10	10	10	28	19	11	21	17	3	2	2
15	11	11	11	11	11	11	29	20	11	22	18	3	2	2
16	12	12	12	12	12	12	30	21	12	22	18	3	2	2

Double-thick Blocks.

6	5	4	6	5	7	18	14	9	14	12	1	1
7	6	5	7	6	8	19	15	9	15	13	1	1
8	6	5	8	6	7	20	15	10	16	14	1	1
9	6	5	9	6	8	21	16	10	16	14	1	1
10	7	6	10	7	9	22	17	10	17	15	1	1
11	7	6	11	7	9	23	18	10	17	15	1	1
12	8	7	12	8	10	24	18	10	18	16	1	1
13	8	7	13	8	10	25	19	10	19	17	1	1
14	9	8	14	9	11	26	20	10	20	18	1	1
15	9	8	15	9	11	27	21	10	21	19	1	1

Treble-thick Blocks.

3	2	1	3	2	7	17	13	15	13	10	2	1
4	3	2	4	3	8	18	13	16	13	11	2	1
5	4	3	5	4	9	19	14	17	14	12	2	1
6	5	4	6	5	10	20	15	18	15	13	2	1
7	6	5	7	6	11	21	16	19	16	14	2	1
8	7	6	8	7	12	22	16	20	16	15	2	1
9	8	7	9	8	13	23	17	21	17	16	2	1
10	9	8	10	9	14	24	18	22	18	17	2	1
11	10	9	11	10	15	25	19	23	19	18	2	1
12	11	10	12	11	16	26	20	24	20	19	2	1
13	12	11	13	12	17	27	21	25	21	20	2	1
14	13	12	14	13	18	28	22	26	22	21	2	1
15	14	13	15	14	19	29	23	27	23	22	2	1
16	15	14	16	15	20	30	24	28	24	23	2	1

TABLE OF THE DIMENSIONS OF SHIPS' BLOCKS (in Inches)—
continued.

Long-tackle Blocks.

Length of Block	Breadth of Upper Block	Breadth of Lower Block	Thickness of Block	Diameter of Upper Sheave	Diameter of Lower Sheave	Thickness of Shafts	Length of Upper Mortice	Length of Lower Mortice	Thickness of Mortice	Size of Pin-hole
10	4	3	3	3	2	1	5	4	1	1
11	5	4	3	4	3	1	5	4	1	1
12	5	4	3	4	3	1	5	4	1	1
13	6	5	3	5	4	1	6	5	1	1
14	6	5	3	5	4	1	6	5	1	1
15	7	6	3	6	5	1	7	6	1	1
16	7	6	3	6	5	1	7	6	1	1
17	8	7	4	7	6	1	8	7	1	1
18	8	7	4	7	6	1	8	7	1	1
19	9	8	4	8	7	1	9	8	1	1
20	9	8	4	8	7	1	9	8	1	1
21	10	9	4	9	8	1	10	9	1	1
22	10	9	4	9	8	1	10	9	1	1
23	11	10	4	10	9	1	11	10	1	1
24	11	10	4	10	9	1	11	10	1	1
25	12	11	4	11	10	1	12	11	1	1
26	12	11	4	11	10	1	12	11	1	1
27	13	12	4	12	11	1	13	12	1	1
28	13	12	4	12	11	1	13	12	1	1
29	14	13	4	13	12	1	14	13	1	1
30	14	13	4	13	12	1	14	13	1	1

Top-sail-sheet Blocks.

Length of Block	Breadth of Block	Thickness of Block	Length of Mortice	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole	Length of Block	Breadth of Block	Thickness of Block	Length of Mortice	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole
6	4	3	4	3	1	1	13	10	6	10	8	1	1
7	5	3	5	4	1	1	14	10	6	10	8	1	1
8	5	3	5	4	1	1	15	11	6	11	9	1	1
9	6	4	6	5	1	1	16	12	7	12	9	1	1
10	6	4	6	5	1	1	17	13	7	13	10	1	1
11	7	5	7	6	1	1	18	13	8	14	10	1	1
12	7	5	7	6	1	1	19	14	8	15	11	1	1

Nine-pin Blocks.

Length of Block	Breadth of Block	Thickness of Block	Length of Mortice	Diameter of Sheave	Thickness of Sheave	Length of Pin	Length of Block	Breadth of Block	Thickness of Block	Length of Mortice	Diameter of Sheave	Thickness of Sheave	Length of Pin
8	5	4	6	4	1	5	11	6	5	7	5	1	7
9	5	4	6	4	1	5	12	7	5	8	6	1	8
10	6	5	7	5	1	6	13	8	6	9	7	1	9
11	6	5	7	5	1	6	14	9	6	10	8	1	10
12	7	6	8	6	1	7	15	10	7	11	9	1	11
13	7	6	8	6	1	7	16	11	8	12	10	1	12
14	8	7	9	7	1	8	17	12	9	13	11	1	13
15	8	7	9	7	1	8	18	13	10	14	12	1	14
16	9	8	10	8	1	9	19	14	11	15	13	1	15

TABLE OF THE DIMENSIONS OF SHIPS' BLOCKS (in Inches)—
continued.

Snatch Blocks.

Length of Block	Breadth of Block	Thickness of Block	Length of Mortice	Thickness of Mortice	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole	Length of Block	Breadth of Block	Thickness of Block	Length of Mortice	Thickness of Mortice	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole
7	3	3	5	1	3	3	1	17	9	7	11	2	7	3	1
8	4	3	5	1	3	3	1	18	10	7	11	2	7	3	1
9	4	3	5	1	3	3	1	19	10	8	12	2	8	3	1
10	5	4	6	1	4	4	1	20	11	8	13	2	8	3	1
11	5	4	6	1	4	4	1	21	11	9	14	3	9	3	1
12	6	5	7	1	5	5	1	22	12	9	14	3	10	3	1
13	6	5	7	1	5	5	1	23	12	10	15	3	10	3	1
14	7	6	8	1	6	6	1	24	13	10	16	3	11	3	1
15	7	6	8	1	6	6	1	25	13	10	16	3	11	3	1
16	8	7	9	1	7	7	1	26	14	11	17	3	12	3	1

Single-sister Blocks.

Length of Block	Diameter of Block	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole	Length of Block	Diameter of Block	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole	Length of Block	Diameter of Block	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole
6	3	3	3	1	7	4	4	3	1	9	4	4	4	2
8	3	3	3	1	8	4	4	3	1	10	4	4	4	2
10	3	3	3	1	10	4	4	3	1	12	4	4	4	2
12	3	3	3	1	12	4	4	3	1	14	4	4	4	2
14	3	3	3	1	14	4	4	3	1	16	4	4	4	2
16	3	3	3	1	16	4	4	3	1	18	4	4	4	2

Double-sister Blocks.

Length of Block	Diameter of Block	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole	Length of Block	Diameter of Block	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole	Length of Block	Diameter of Block	Diameter of Sheave	Thickness of Sheave	Size of Pin-hole
10	3	3	3	1	17	5	5	4	1	24	7	7	6	2
11	3	3	3	1	18	5	5	4	1	25	7	7	6	2
12	3	3	3	1	19	5	5	4	1	26	7	7	6	2
13	3	3	3	1	20	5	5	4	1	27	7	7	6	2
14	3	3	3	1	21	5	5	4	1	28	7	7	6	2
15	4	4	4	1	22	6	6	5	1	29	8	8	7	2
16	4	4	4	1	23	6	6	5	1	30	8	8	7	2

Trucks.

Diameter of Truck	Thickness of Truck	No. of Sheaves	Diameter of Truck	Thickness of Truck	No. of Sheaves	Diameter of Truck	Thickness of Truck	No. of Sheaves	Diameter of Truck	Thickness of Truck	No. of Sheaves
5	1	3	6	1	3	7	1	3	8	1	3
6	1	3	7	1	3	9	1	3	10	1	3
7	1	3	8	1	3	11	1	3	12	1	3
8	1	3	9	1	3	13	1	3	14	1	3
9	1	3	10	1	3	15	1	3	16	1	3
10	1	3	11	1	3	17	1	3	18	1	3
11	1	3	12	1	3	19	1	3	20	1	3
12	1	3	13	1	3	21	1	3	22	1	3
13	1	3	14	1	3	23	1	3	24	1	3
14	1	3	15	1	3	25	1	3	26	1	3
15	1	3	16	1	3	27	1	3	28	1	3
16	1	3	17	1	3	29	1	3	30	1	3

Double Double
3 3

TABLE OF THE DIMENSIONS OF SHIPS' BLOCKS (in Inches)—
concluded.

<i>Dead-eyes.</i>											
Length	Breadth	Thickness	Length	Breadth	Thickness	Length	Breadth	Thickness	Length	Breadth	Thickness
5	5	3	9	9	5½	13	13	8	17	17	10
6	6	4	10	10	6½	14	14	8½	18	18	10½
7	7	4½	11	11	7	15	15	9	19	19	11
8	8	5	12	12	7½	16	16	9½	—	—	—

<i>Closed Hearts.</i>											
Length	Breadth	Thickness	Gouging	Length	Breadth	Thickness	Gouging	Length	Breadth	Thickness	Gouging
5	4½	3½	1	9	7½	5	2	13	10	7	2½
6	4¾	3¾	1	10	8	5½	2	14	11	7½	2¾
7	5½	4	1	11	8½	6	2½	15	11	8	3
8	7	4½	1	12	9	6½	2½	16	12	8½	3½

<i>Open Hearts.</i>											
Length	Breadth	Thickness	Gouging	Length	Breadth	Thickness	Gouging	Length	Breadth	Thickness	Gouging
5	4½	3½	1	9	8	6	1	13	12	8	1½
6	5	4	1	10	9	6½	1	14	13	8½	1½
7	6	5	1	11	9½	7	1	15	14	9	1½
8	7	5½	1	12	11	7½	1	16	14½	9	1

TABLE OF THE VALUE OF THE BELGIAN GAUGE IN
DECIMALS OF AN INCH.

Mark	Size	Mark	Size	Mark	Size	Mark	Size	Mark	Size
1	·004	7	·015	13	·034	19	·067	25	·111
2	·006	8	·017	14	·037	20	·074	26	·120
3	·008	9	·019	15	·041	21	·082	—	—
4	·009	10	·022	16	·043	22	·089	—	—
5	·011	11	·026	17	·052	23	·097	—	—
6	·013	12	·030	18	·059	24	·104	—	—

VOCABULARY OF TECHNICAL TERMS USED IN
SHIPBUILDING.

ENGLISH—FRENCH.

Chaff, en arrière	Bitte, bittes
Chord, à bord	Blade of a screw, aile d'hélice
Admiral, amiral	Blister steel, acier poulie
Admiralty, amirauté	Block, poulie, moufle
Alse, herminette	Block and fall, palan
Atlat, à flot	Boarding pike, piqued'abordage
Aft, arrière, de l'arrière	Boat, bateau, canot
Air pump, pompe à air	Boatswain, maître d'équipage
Alee, sous le vent	Bobstay, sous-barbe
Amidships, au milieu du navire	Body plan, plan vertical
Anchor, ancre	Boiler maker, chaudronnier
Angle iron, cornière, fêr d'angle	Boiler plate, tôle
Apron, radier, contre-étrave, platine	Bollard, corps mort
Ash, frêne	Bolt, cheville, boulon
Astern, à l'arrière, de l'arrière	Bolt rope, ralingue
Ashward, par le travers	Boom, bout dehors, arc-boutant
Awning, tente	Bow, l'avant d'un vaisseau
Almuth compass, compas de variation	Bower-anchor, ancre du bossoir
Back of stern-post, contre-étambot	Bowspit, beaupré
Bucketay, galhauban	Brace, bras
Large, grand canot, allège	Bracket, courbaton
Bar iron, fer en barres	Brail, cargue
Barque, barque, bateau	Bread room, soute au pain
Barrel of the capstan, mèche du cabestan	Breadth extreme, plus grande largeur
Barrel of the steering wheel, tambour de la roue du gouvernail	Breaker, brisant, baril de galère
Batten, liteau	Breast-plate, conscience
Beam, bau	Brig, brig
Beech, hêtre	Brigantine, brigantin
Bending press, machine à cintrer les tôles	Bucket, baille
Between-decks, entrepont	Builder, constructeur
Bowel, angle oblique, angle d'équerrage	Bulk head, cloison
Bilge, petit fond d'un navire	Bunker, soute
Bilge pump, pompe de cale	Bunt-line, cargue-fond
Bilge ways, coittes	Buoy, bouée, balise
Binnacle, habitacle	Buoyant, léger, émergé
	Burton, petit palan
	Butt, about, tête d'un couple
	Butt cover, plaque de jonction d'écart de tôle
	Cabin, cabine, chambre, lit
	Cable, câble
	Cable tier, fosse aux câbles

TABLE OF THE STRENGTH OF LONG COLUMNS WHOSE LENGTH EXCEEDS THIRTY TIMES THEIR DIAMETER.

W = breaking weight in tons. L = length in feet. D = external diameter in inches. d = internal diameter in inches.

Kind of Column	Both Ends Rounded	Both Ends Flat
Hollow cast-iron cylindrical pillars	$W = 13 \frac{D^{3.75} - d^{3.75}}{L^{1.75}}$	$W = 44.34 \frac{D^{3.75} - d^{3.75}}{L^{1.75}}$
Solid cast-iron cylindrical pillars	$W = 14.9 \frac{D^{3.75}}{L^{1.75}}$	$W = 44.16 \frac{D^{3.75}}{L^{1.75}}$
Solid wrought-iron cylindrical pillars	$W = 42.8 \frac{D^{3.75}}{L^{1.75}}$	$W = 123.78 \frac{D^{3.75}}{L^{1.75}}$
Solid square pillars of dry deal	—	$W = 7.81 \frac{D^4}{L^2}$
Solid square pillars of dry Dantzic oak	—	$W = 10.96 \frac{D^4}{L^2}$

STRENGTH OF SHORT COLUMNS.

W = breaking weight of long column of same diameter.

w = breaking weight of short column.

C = crushing force of materials in tons $\times$ sectional area of column.

$$w = \frac{WC}{W + \frac{1}{2}C}$$

RIVETED JOINTS.

t = thickness of plate in inches.

d = diameter of rivet in inches.

p = pitch or distance from centre to centre of rivet.

n = number of rows of rivets.

$$p = d + \frac{7854d^2}{t}$$

$$n = \frac{(p-d)t}{7854d^2}$$

Notes.—Each plate is weakened by the rivet holes in the ratio

$$\frac{p-d}{p} = \frac{7854d^2}{t + 7854nd}$$

TABLE OF DIMENSIONS OF RIVETS GENERALLY USED.

Thickness of Plates in Inches	Diameter of Rivets in Inches			London	
	Lloyds	Liverpool Registry	Admiralty	Diameter of Rivets in Inches	Length Counter-sunk in Inches
$\frac{1}{16}$	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
$\frac{1}{8}$	$\frac{3}{8}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
$\frac{1}{4}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
$\frac{3}{8}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
$\frac{1}{2}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
$\frac{5}{8}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
$\frac{3}{4}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
$\frac{7}{8}$	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$
1	$\frac{3}{4}$	$\frac{1}{2}$	$\frac{1}{2}$	$\frac{1}{8}$	$1\frac{1}{2}$

Note.—Lloyds require a spacing of $4\frac{1}{2}$ diameters.

Liverpool Registry require a spacing of 4 diameters.

Admiralty require a spacing of $4\frac{1}{2}$ to 5 diameters in edges and butts of bottom plating and bulkhead plating, and 5 to 6 diameters in water-tight work elsewhere.

Veritas require a spacing of 4 diameters for single-riveting and $4\frac{1}{2}$ diameters for double-riveting.

NOTES ON RIVETED JOINTS.

1. A closer pitch of rivets should be adopted in single- than in double-riveted butts and in double- than in treble-riveted butts.
2. With a 4-diameter pitch the efficiency of a single-riveted butt is very small.
3. With a 4-diameter pitch the strength of a double-riveted butt is about at the maximum when the plates are not more than $\frac{1}{2}$ in. thick.
4. When plates are more than $\frac{3}{4}$ in. thick larger rivets should be put in than those generally in use.

BUTT STRAPS.

Fig. 153.

In joints of the character shown in the diagram the strength of the plates joined is only weakened to the extent caused by cutting away a width equal to the diameter of one rivet.

